Long term performance prediction of existing PVC water distribution systems

**TNO Science and Industry** 

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## Introduction

- PVC water pipes have been in service since 1950's
- It was assumed that these pipes have a lifetime of approx. 50 year
- Question: "Do PVC pipes have to be replaced after 50 years or can they last longer?"

#### Objective:

development of reliable methods for prediction of residual lifetime of PVC water distribution systems based on a thorough understanding of underlying degradation processes which is accepted within PVC pipe industry and PVC water pipe users



# Introduction

#### Sponsors

- water distribution companies by Kiwa
- PVC pipe manufacturers (Dyka, Pipelife, Wavin)
- PVC raw material producers (LVM, Shin-Etsu, Solvay)
- TNO (Netherlands organisation for applied scientific research)
- TNO Science and Industry (1 of 5 TNO institutes)
  - Materials Technology (1 of 8 departments)
    - Product assessment, durability and stabilisation





## Introduction

#### Development of water distribution systems





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## **Degradation and failure processes in PVC**

- Chemical degradation:
  - Change in chemical structure of the polymer
- Physical ageing
  - Change in physical structure of the polymer
- Mechanical damage:
  - Craze initiation and crack growth as a result of internal and external stresses may lead to ultimate pipe failure



# **Chemical ageing**

- Degradation mechanism:
  - Dehydrochlorination and thermo-oxidation
  - HCl is released influenced by thermal energy
    - Slow in service at 15 °C
    - Fast during processing at 200 °C
- Consequence:
  - Embrittlement
  - Discoloration
- Chemical physical checks:
  - K-value
  - residual amount of stabiliser
  - concentration of vinyl group

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# **Chemical ageing**

- Degradation kinetics from DHC experiments at elevated temperatures
- Most negative scenario indicates that at 10 °C the K-value decreases from 66 to 65
- Higher temperatures causes an accelerated degradation rate





## **Chemical ageing**

- Modelling of chemical degradation indicates that the increase of the degree of degradation after 100 years at 15 °C is significantly smaller than is caused by processing
- Conclusion:
- Chemical ageing at 15 °C seems not to have a significant influence the quality of PVC water distribution pipes



#### • Ageing mechanism

- Free volume relaxation (compacting of polymer)
- Temperature dependent
  - Slow in service at 15 °C
  - Fast during cooling after extrusion of the pipes

#### • Consequences

- Increase in craze initiation stress
- Increase probability for crack growth after initiation
- Increase in burst strength
- Lower elongation at break
- Physical check:
  - Measurement of yield stress in stress-strain experiment



- Accelerated ageing of new PVC pipe at 60 °C leads to an increase in yield stress
- Expectation:

The yield stress is an indication for the age of the excavated pipe









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- Yield stress depends on wall thickness and not on age
- Thicker wall cools more slowly and generates more physical ageing
- The state of physical ageing is determined immediately after production and hardly changes in service
- Conclusion:
- Physical ageing at 15 °C seems not to have a significant influence on the quality of water distribution pipes



#### **Mechanical failure**

- Initiation of crazes and cracks under the influence of external stresses
- Presence of damage and particles accelerates failure
- Deformation of the surrounding soil
- Internal water pressure
- Water hammer
- Traffic load





## **Failure mechanism**

- Constant or peak load can lead to:
  - Craze initiation
  - Craze growth
  - Crack formation
  - Crack growth
- And ultimately to:
  - Pipe failure





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#### **External conditions**

- PVC raw material
- Additives (stabilisers; pigments;...)
- Processing conditions (temperature, residence time in extruder; degree gelation; cooling rate; ...)
- Internal stresses (size; relaxation; ...)
- Damages (scratches; "spider lines"; inhomogeneities; ...)
- Mechanical loads (installation; water pressure; water hammer; soil; ...)
- Effect of environmental conditions (temperature; UV; chemicals, ...)



### **Experimental validation**

- Constant loading
  - Craze initiation on tapered samples
  - Slow crack growth on small ting samples
  - Burst pressure on whole pipe segments
- Occasional loading
  - Fatigue loading of rings



## **Experimental validation**

• Excavated pipes

| Production | Diameter | Wall      | K-value | Degree of |
|------------|----------|-----------|---------|-----------|
| year       | (mm)     | thickness |         | gelation  |
|            |          | (mm)      |         | (%)       |
| 1959       | 200      | 7.6       | 71      | 58        |
| 1970       | 500      | 15.6      | 67      | 39        |
| 1975       | 315      | 9.7       | 64      | 38        |
| 1984       | 400      | 12.7      | 66      | 55        |
| 1997       | 160      | 4.8       | 67      | 80        |
| 2003       | 160      | 4.3       | 68      | 70        |



• Tapered samples are stressed and the time until the formation of crazes is monitored





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Annealing of pipes at 60 °C increases physical ageing

Physically aged pipes have a higher resistance against the formation of crazes





Craze initiation stress does not depend on the age of the pipe



• Craze initiation stress level after 100 year service life at 20 °C

| Production | Stress level | Uncertainty |
|------------|--------------|-------------|
| year       | (MPa)        | (MPa)       |
| 1959       | 14.3         | 2.1         |
| 1970       | 17.4         | 2.0         |
| 1975       | 16.9         | 0.9         |
| 1984       | 15.7         | 0.9         |
| 1997       | 21.4         | 2.7         |
| 2003       | 12.8         | 0.5         |

Critical values in view of the design pressure of 12.5 MPa



#### **Burst pressure**

• Pipes are hydrostatically pressurised and the time until failure is monitored





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All (excavated) pipes show a similar burst pressure behaviour Ageing at 60 °C increases the resistance against internal water pressure



#### **Burst pressure**

• Burst pressure stress level after 100 year service life at 20 °C

| Production | Stress level | Uncertainty |
|------------|--------------|-------------|
| year       | (MPa)        | (MPa)       |
| 1959       | 27.0         | 0.5         |
| 1970       | 20.7         | 0.5         |
| 1975       | 23.0         | 0.9         |
| 1984       | 24.3         | 1.4         |
| 1997       | 26.3         | 0.6         |
| 2003       | 28.4         | 0.6         |

Critical values in view of the design pressure of 12.5 MPa



- Ring segment is notched and subjected to three point bending
- The time until failure is monitored versus applied stress









#### **Ductile failure**

#### **Brittle failure**



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- All excavated pipes fail in a ductile manner
- Failure behaviour is comparable to burst pressure behaviour
- However, pipes of 1970, 1975 and 1984 show significant scatter in results
  - Low degree of gelation
  - Larger particles
- Extrapolation to 12.5 MPa for these pipes gives large uncertainty



• Slow crack stress level after 100 year service life at 20 °C

| Production | Stress level | Uncertainty |
|------------|--------------|-------------|
| year       | (MPa)        | (MPa)       |
| 1959       | 26.7         | 1.9         |
| 1970       | 17.3         | 5.0         |
| 1975       | 19.7         | 6.3         |
| 1984       | 24.4         | 7.1         |
| 1997       | 22.1         | 4.7         |
| 2003       | 21.1         | 2.2         |

Critical values in view of the design pressure of 12.5 MPa



## Fatigue

- Loaded ring is rotated
- Number of cycles until failure is monitored versus stress level applied







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## Fatigue





# Fatigue

Fatigue stress level that can be withstand for 10<sup>7</sup> cycles in 100 years at 20 °C (=10/hour)

| Production | Stress level | Uncertainty |
|------------|--------------|-------------|
| year       | (MPa)        | (MPa)       |
| 1959       | 8.0          | 1.7         |
| 1970       | 4.1          | 1.7         |
| 1975       | 4.0          | 1.0         |
| 1984       | 5.5          | 1.7         |
| 1997       | 13.6         | 4.4         |
| 2003       | 8.9          | 1.4         |

• This means a deflection < 2% for the 1970, 1975 and 1984 pipes

Critical values in view of traffic load



### Conclusions

• Prediction service life of currently produced PVC water distribution pipes with the high quality control procedures on material, processing and stabilisation applied by Dyka, Pipelife and Wavin

#### > 100 years

- *Provided:* good control during construction activities and service e.g.
  - Back fill of soil
  - Soil settlements
  - Water pressure
  - Magnitude and occurrence of water hammer
  - Ground works



### Conclusions

• Residual service life of PVC water distribution pipes in service not restricted to 50 years

• Residual service time determined by:

- Material properties
- Stabiliser package
- External load of soil and traffic
- Water pressure (water hammer)
- Ground works
- New connections
- Unforeseen conditions



#### **Unforeseen conditions**





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